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Satellite session

# **ECO Driving of E-bus**

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# AGENDA

- Polygon testing, Investigation of the influence of E-bus driving style on energy efficiency, comparise polygon test/simulation
- Real exploitation, Research of influencing factors on the electricity consumption of E-buses



The question Why polygon testing ?



# **POLYGON TESTING**

The answer: The best way to research Controlled conditions:

- defined length of the test track
- defined driving cycle
- without influence from other vehicles, traffic light
- one test driver, different ways of accelerating and braking the E-bus
- repeatability of the test
- the same mass of vehicles
- Provided optimal operating voltage of supercapacitor, the maximum voltage drop was up to 10 % of the voltage value after charging (575 V), charger nearby,

Results from the polygon are the best way of verification of simulation results





### Project: Research on the efect of driving style on energy efficiency of electric buses

Client of the project City Administration Belgrade-Secretariat for Public Transport

Project leader: Prof. Ivan Blagojevic\*, PhD

Researchers: Blagojevic I\*, Stamenkovic D\*, Ivankovic I\*, Milicic B\*, Maljkovic M\*, Frlic N\*, Zunjic M\*, Mišanović S \*\*, Ivanov S\*\*

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#### Table 1 Characteristics of polygon sections

Section	Lenght [m]	Rise/fall [%]
Р	295	0,00
M	310	-0,3
В	280	-0,7





Figure 2 Polygon with test sections



Figure 1, Test section ''M''

# **POLYGON TESTING**

## E-bus, Higer KLQ6125GEV3 Ultracapacitor tehnology



Figure 3 Higer KLQ6125GEV3



Figure 4 Higer KLQ6125GEV3

#### **Technical Data**

Manufacturer	Higer
Туре	Electric KLQ6125GEV3
Length / width / height	12000/2550/3680 mm
Curb weight	12540 kg
Passengers	
Max.speed	
Charaing the terminus: 660 V DC or 380 V	AC. 580 V DC output. 250 A
Charging time at the terminus	
Storage system	super capacitors
Capacity	20 kWh
Manufacturer	Aowei
Type	U-CAP (37DT6-03210)
Traction motors	
Manufacturer	Siemens
Type	
Power	
Torque	
Inverter	DC / AC
Manufacturer	Zhonalian
Type	IEVD 130-60ZO6GA
Working range	580 V DC / AC 500-650V
Convereter	DC / DC
Manufacturer	Zhonalian
Туре	DY074C
Working range	12-24-48 V DC
Charging system:	
Pantograph	Aowei 37DT6-03212
Plug-in	DUOSIDA 37XL2 -3709
Auxiliary systems:	
Air conditioning	Thermoking 81DT6
Pump control	KVD HDZXB 1416
Compressor	IEM ER 230
UC-Cooler	Aowei 37DT6
Traction control	Siemens 10DT6
External display	Novatronic



# **POLYGON TESTING**

## Vehicle load

The vehicle is to be loaded with 50% of maximum payload, because at that time the load corresponds with SORT metodologys. The load can be achieved by evenly distributed sand bags of 40 kg each (total mass of 3060 kg), which corresponds with the mass of 45 passengers of 68 kg each (Figure 5). In each mode of testing and load, there are 3-7 examiners in the vehicle as well (total max.mass of 490 kg).



Figure 5 Vehicle load





### **Representative driving cycles**

Based on the lengths of the test tracks (P, M, B), the basic driving cycle is defined, which includes the phases: acceleration, constant speed, deceleration. The maximum speed that was achieved was between 40 and 45 km / h.







## **Acceleration modes**

Accelerator pedal position is the parameter according to which the driver inflicts the acceleration intensity. Therefore the testing of acceleration modes should cover constant accelerator pedal position, as well as variable accelerator pedal positions. To overcome the subjectivity problem, the way to inflict different accelerations that the driver is supposed to follow is implemented. According to Figure 7, several curves were established, each representing the change in speed during time spent to accomplish the same maximum value, defined by the equation:

$$v = v_0 + (v_f - v_0)(\frac{t - t_0}{t_f - t_0})^{\beta}$$

where:

- v, $v_0$ ,vf - current, initial and final speed [m/s]

Curves were obtained by adopting different values of coefficient  $\beta$  ( $\beta$ =0.7, 0.85, 1.4), where the coefficients less than 1 form convex curves, and coefficients greater than 1 form concave curves.





The driver can track speed via defined curves as shown on a tablet computer, so that the speed change over time dictates current position of acceleration pedal. During trial testing, it was observed that the curves defined by coefficient  $\beta < 0.7$  were not reachable due to the limits of dynamic characteristic of the vehicle. Likewise, it was founded that when the coefficient is greater than 2, the vehicle needs a large amount of time to reach the desired speed, which is by no means energy efficient.



The driver can track speed via defined curves as shown on a tablet computer, so that the speed change over time dictates current position of acceleration pedal.





Figure 8 Tablet computer with curves



### **Constant speed modes**

Testing is performed for different values of maximum speeds in the range from 40 to 45 km / h. Due to the limited length of the test track, the achieved speed was usually maintained between 2-4 seconds.

### **Deceleration modes**

Low, medium, and high deceleration intensities, with the vehicle loaded and unladen, to determine the amount of energy recovered for the various accelerator pedal positions, load conditions, and speeds before and during the braking process



# **POLYGON TESTING**

## **Measuring equipment**

- HBM QuantumX MKS840A, measuring and acquisition device
- MTN / 7100 monitor, acceleration sensor
- Racelogic-Vbok, GPS speed sensor
- Fujitsu Lifebook E series, laptop
- Samsung Galaxy Tab A, Laptop (Figure 8)
- Catman AP V.3.5.1, data processing software package



Figure 9 Measuring equipment





# **POLYGON TESTING**

# Bus parameters monitored during testing and the way of their quantifying and obtaining

Acquisition of desired parameters of electric bus is done by **V-CAN** and **S-CAN** output on CAN and selected analogue signals. Parameters monitored during testing:

Supercapacitor state of charge: AW \_SOC\_ [%]

Motor torque: Actual Drive Motor Torque [%]

Accelerator pedal position: AP Position [%]

Brake pedal position: Brake Pedal Position [%]

Motor speed: Drive Motor Speed [rpm]

Several parameters are monitored over analogue signals in such manner that the cables are connected on data acquisition unit from adequate supercapacitor connection points:

Supercapacitor current: I\_UC [A]

Supercapacitor voltage: U\_uc [V]

**Invertor current**: I\_inv [A]

Longitudinal acceleration over separate sensor: Monitran [g]

In order to check vehicle speed accuracy acquired over CAN, the speed sensor based on GPS and GLONASS signals is used. Data acquisition sampling rate was set to 50 Hz, except for vehicle speed measured via sensor, where it was set to 5 Hz.



### Determination of consumed and recuperated energy

The consumed ( $E_{p_{uc}}$ ) and recovery ( $E_{r_{uc}}$ ) electricity from/in the supercapacitor [kWh] is calculated on the basis of analogously measured values of current ( $I_{p_{uc}}$ ,  $I_{r_{uc}}$ ) and voltage ( $U_{uc}$ ) in the observed time interval.

The energy consumed can be observed for any vehicle speed measured during the cycle. The regenerated energy is calculated for the braking period, which means from the moment the driver presses the brake pedal to the stop based on the current values of voltage and current flowing into the supercapacitor. The start and end of braking are determined based on the current position of the brake pedal. Recovery efficiency is expressed by the recovery efficiency coefficient ( $\lambda_{uc}$ ) as the ratio of electricity returned to the supercapacitor ( $E_{r_{uc}}$ ) and electricity taken from the supercapacitor ( $E_{p_{uc}}$ ) in the observed time period.

$$E_{p_{uc}} = \sum_{s=1}^{m} \frac{\int_{t_{ps}}^{t_{ks}} U_{uc} \cdot I_{p_{uc}} \cdot dt}{3600000} , \qquad (kWh)$$

$$E_{r_{uc}} = \sum_{s=1}^{p} \frac{\int_{t_{prs}}^{t_{krs}} U_{uc} \cdot I_{r_{uc}} \cdot dt}{3600000} , \qquad (kWh)$$

$$A_{uc} = \frac{E_{r_{uc}}}{E_{p_{uc}}} \cdot 100 , \qquad (\%)$$



# **POLYGON TESTING**

**Results analysis** 

- During Phase 1 of the project, there were three test days: November 15th, December 4th, and December 17th, 2019.
- Each cycle on a single section consists of a single planned acceleration mode for different values of coefficient β, after which follows the appropriate deceleration mode.
- Due to the nature of testing, it was necessary to repeat cycles on all sections ("P", "M", and "B").
- The effect of the state of charge of a supercapacitor is minimized with frequent charging, to exclude the effect of voltage change on the energy consumed.
- In all three aforementioned methods of proving ground testing, over 100 cycles were driven.
- Based on the described method of data analysis and calculation of consumed and recuperated energy during a cycle.





 The table for 6 chosen characteristic cycles (out of a total of 27) on the with the loaded vehicle are made, with a maximum speed of 40 km/h.

		Energy consumed	Energy		Supercapacitor voltage in the	
	Cycle number/	until speed of 40	recuperated	Recovery	beginning (Uucp) and in the end	Parameter of
Section (max,min)	section	km/h [kWh]	during braking	efficiency $\lambda_{uc}$	(Uuck) of	characteristics of
			[kWh]	[%]	cycle [v]	acceleration [-]
B, max	27/B	Epuc40 = 0.367	Eruc = 0.139	37.8	Uucp, Uuck = 535, 516	β ≈ 0.7
B, min	9/B	Epuc40 = 0.389	Eruc = 0.094	24.1	Uucp, Uuck = 546, 526	β ≈ 0.85
P, max	16/P	Epuct40 = 0.384	Eruc = 0.125	32.5	Uucp, Uuck = 560, 540	β ≈ 1.4
P, min	13/P	Epuc40 = 0.410	Eruc = 0.093	22.6	Uucp, Uuck = 576, 560	-
M, max	14/M	Epuc40 = 0.386	Eruc = 0.121	31.3	Uucp, Uuck = 573, 553	β ≈ 1.4
M, min	8/M	Epuc40 = 0.399	Eruc = 0.095	23.8	Uucp, Uuck = 554, 533	β ≈ 0.85

Polygon test, Section ''B''  $\lambda_{uc-max} = 37.8 \%$ ,  $\lambda_{uc-min} = 24.1 \%$ 

Value  $\lambda_{uc}$  (%), the direct influence of the driving style

Real operation: all influencing factors:

\*line EKO1, direction ''A''  $\lambda_{uc-max} = 28.55\%$ ,  $\lambda_{uc-min} = 16.75\%$ , average 22.9% \*line EKO1, direction ''B''  $\lambda_{uc-max} = 19.57\%$ ,  $\lambda_{uc-min} = 9.84\%$ , average 13.9%



<sup>\*</sup>Misanovic S.: Energy and environmental performance of E-bus in the passenger transport system, doctoral dissertation, Faculty of Engineering, University of Kragujevac, 2021









# POLYGON TESTING Recommendations

Based on the analysis of the results, the following recommendations were defined:

- In constant speed driving mode, the optimal value of speed is around 35 km/h. This was confirmed by the geometric place of points in the efficiency map.
- In acceleration modes, the accelerator pedal is to be pressed by a continual rate (positive or negative), and its position is not to oscillate. If the desired speed is reached by alternating the increase and decrease in the pedal position, the energy efficiency is far worse, as was confirmed by the tests and proven by geometric place of points in the efficiency map during the acceleration (more points are placed in lower efficiency region), as well as by the effect of rotating masses of drivetrain and transmission, and also the inertia of the whole vehicle. In case the driver accomplishes requested acceleration by continual position change of accelerator pedal, there are no aforementioned oscillations, so the seemingly inefficient cycle of maximum acceleration gives the best effect. Anyways, the stated effect would be even higher if the maximum deflection of the pedal is reached by its continual, and not abrupt change.
- Brake pedal, if the traffic allows, is to be kept in the interval from 0 to 28% of maximum position, which would permit only the regenerative braking in the range up to maximum brake torque of electric motor or generator.
- Energy is recuperated without braking, by means of vehicle inertia (regenerative torque is 34 Nm) in which case the time and length of travel where the energy recuperation occurs is extended.



# **POLYGON TESTING**

- Based on the recommendations for E-bus the ideal cycle between two stops consists of a mode of continuous acceleration and deceleration by inertia and/or braking within the recommended limits.
- This cycle differs from the recommended cycle for a bus with an internal combustion engine, for the same distance traveled
- The recommended driving style implies that the section between the two stops must be approved in order for the cycle to be reported. This can be applied in special lanes (corridor) intended exclusively for buses with prior driver training



Figure 15 Recommended driving cycle based on speed between two stops for the case of electric bus (right) and internal combustion engine bus (left)



# **VERIFICATION OF SIMULATION RESULTS**

#### **Modelinig and Simulation**

- Driving cycle modeling (acceleration, Vmax, V-const, deceleration)
- Technical characteristics E-bus, Higer KLQ6125GEV3
- Fundamentals of vehicle motion theory, Resistance, Power, Energy, calculation
- Specifics of the theory of regenerative braking of E-buses and electricity recovery (generator mode of electric motors)



Figure 16 E-bus, Resistances



# **VERIFICATION OF SIMULATION RESULTS\***

#### \*Real driving cycle on poligon, section ''B''

	duration	distance
	(s)	(m)
Acceleration	16.79	126.26
Constant speed, v <sub>const</sub> =44 km·h <sup>-1</sup>	3.68	44.94
Braking	15.81	100.69
Total	36.28	271.89

#### \*Measurement results

ν <sub>max,</sub> km · h⁻¹	44
$m{E}_{m{p}_{m{u}c}}$ , kWh	0.4700
$m{E}_{m{r_{uc}}}$ , kWh	0.1390
$\lambda_{uc}$ , %	29.57



Theoretical cycle  $\beta = 1$  ( $\alpha = const = 0.72 \text{ m/s2}$ ), deceleration b=const=0.77 m/s2 Max.driv. cycle ( $\alpha$ -variable,  $\alpha$ min=0.51m/s2  $\alpha$ max=1.73 m/s2) (b-variable, bmin=0.65m/s2 bmax=0.87 m/s2

#### Figure 17



# **VERIFICATION OF SIMULATION RESULTS**

## Driving cycles, Simulation\*





#### Figure 18 current acceleration, simulation

 $a'_{ebus} = \text{RAND}() \cdot (a_{ebus_{max}} - a_{ebus_{min}}) + a_{ebus_{min}}$ 



 $b_{ebus}^{'} = \text{RAND}() \cdot (b_{ebus_{max}} - b_{ebus_{min}}) + b_{ebus_{min}}$ ,

# **VERIFICATION OF SIMULATION RESULTS**

### **Results of Simulations\***

$a_1 = -44$ km b·1 $\mu = 0.797$	Distance	E <sub>puc</sub>	E <sub>ruc</sub>	λ <sub>uc</sub>
<i>V<sub>max</sub>=44</i> Km 11 <sup>-</sup> , 0=-0,776	m	kWh	kWh	%
Teoretical driving cycle $\beta$ =1	244,23	0,4608	0,1356	29,43
Max.driving cycle	283,7	0,4716	0,1321	28,01
Simulation 1	271,75	0,4692	0,1375	29,31
Simulation 2	252,83	0,4631	0,1364	29,45
Simulation 3	273,91	0,4699	0,1376	29,28
Simulation 4	269,61	0,4684	0,1371	29,27
Simulation 5	261,45	0,4654	0,1368	29,39
Simulation 6	268,72	0,4681	0,1371	29,29
Simulation 7	260,79	0,4649	0,1379	29,66
Simulation 8	266,11	0,4668	0,1367	29,28
Simulation 9	267,47	0,4665	0,1352	28,98

	Maggurapant	Simulation	
	Measurement	"7"	
$oldsymbol{v_{max}}$ km ·h⁻¹	44	44	
$E_{p_{uc}}(v_{max})$ , kWh	0.4700	0.4649	
<b>E</b> <sub>rµc'</sub> kWh	0.1390	0.1379	
$\lambda_{uc}$ , %	29.57	29.66	



Figure 21 Simulations 7



\*Misanovic S.: Energy and environmental performance of E-bus in the passenger transport system, doctoral dissertation, Faculty of Engineering, University of Kragujevac, 2021



### Research of influencing factors on the electricity consumption of E-buses

E-bus, consumers	Impact on consumption:			
Electric drive motor	<ul> <li>Driving cycle: (acceleration, speed, number of stations, number of stops</li> <li>Load (number of passengers in the vehicle)</li> <li>Topography of the route</li> <li>Driving style (eco style, moderate, aggressive)</li> <li>E-bus performances (empty vehicle weight, aerodynamics)</li> <li>Losses (electric motor, inverter, cables, battery, charger,</li> </ul>			
Auxiliary devices	<ul> <li>Compressor</li> <li>Steering pump</li> <li>Exterior and interior lighting, displays</li> <li>Low voltage E-bus installation</li> </ul>			
E-bus heating system	Seasonal-winter (outside temperature)			
E-bus cooling system	Seasonal-summer (outside temperature)			





### Line EKO 1 Belgrade



The mean length of the EKO 1 line is 7.98 km. (Direction ''A'' 7,47 km, Direction ''B'' 8.5 km ) The line with a flat configuration with a slight climb





#### Gauss (normal) distribution

#### Review of a sample of E-bus consumption, \*

Direction	''A''
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Direction "B"

Period	Direction	Direction	Direction "A" + "B"	
	''A''	"B"		
Spring- autumn	357	347	704	
Summer	401	453	854	
Winter	397	392	789	
Total	1155	1192	2347	



 $\chi^2$  – chi square test

\*Misanovic S.: Energy and environmental performance of E-bus in the passenger transport system, doctoral dissertation, Faculty of Engineering, University of Kragujevac, 2021





### Analysis commercial speed

\*Spring-autumn period, direction A, EKO 1 line



#### \*Spring-autumn period, direction B, EKO 1 line





#### \*Electricity consumption and commercial speed of e-bus, direction "A", spring-autumn period

# \*Dependence of electricity consumption and commercial speed of E-bus, direction "A", spring-autumn period







\*Electricity consumption and commercial speed, direction "B", spring-autumn period

\*Dependence of electricity consumption and commercial speed of E-bus, direction "B", spring-autumn period





\*Average consumption electricity of E-bus, during daily operation, springautman period, line EKO 1, Impact (Load+speed+rise/fall ) of the route

'Average consumption 'Average consumption Caracteristic period of Caracteristic period of electricity of E-bus Sample electricity of E-bus Sample **E-bus operation E-bus operation** kWh · km<sup>-1</sup> kWh · km<sup>-1</sup> 22 First departures 1,212 24 First departures 0.943 71 Morning peak 1.393 Morning peak 64 1,112 Intermediate-peak load 82 1.354 Intermediate-peak load 81 1.043 Afternoon peak 86 1,523 91 Afternoon peak 1.209 **Evenning** load 72 1.337 71 **Evenning** load 1.049 Last departures 14 1.223 Last departures 26 0.977 347 1.386 Total 357 1.087 Total

Direction "A"

'Average consumption electricity of E-bus, losses in the charging phase are included

#### Direction "B"





\*Spring/autman period, outside temperature and consumption



**Direction** "A"

Direction ''B''

() optimal consumption electricity of E-bus, depending on the outside temperature





### \*Summer period, outside temperatures 16:38 °C and consumption



Direction ''A''





#### \*Winter period, outside temperatures over -12 ÷ 12 °C and consumption



Direction "A"





### \*Auxiliary devices



	Max.Power
Auxiliary devices	[kW]
DC / DC converter, instrument panel low voltage installation 24 V, lighting, signaling, displays	0.9
Air compressor	3.00
Steering hydro pumps	3.00
Total	6.9

Average (all auxiliary devices)	3.1 - 3.9 kW
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#### Electric motor to drive the air compressor



Electric motor for drive steering drive hydro pumps





displays











### \*all factors: period of operation, speed, rise/fall, AC, heating...







# **QUESTIONS?**



# THANK YOU!











